

半橋式設計

輸入最大電壓 Vinmax(V):	12		
中心輸入電壓 Vin(V):	12		
輸入最小電壓 Vinmin(V):	12		
輸出電壓 Vo(V):	50	輸出電壓 Vo(V):	0
輸出電壓 Vo(V):	0	輸出電壓 Vo(V):	0
輸出電流 Io(A):	5	輸出電流 Io(A):	0.25
輸出電流 Io(A):	0.25	輸出電流 Io(A):	0.18
工作頻率 f(Hz):	50000		
工作週期 D(us):	0.3	或 導通時間 Ton(us):	6
大電流-低電壓輸出線路壓降倍數:	1 (10V以下,50A以上輸入 1.11)		
線路壓降 V _{DF} (V):	0.6		
電壓調整率 α:	2.81%		
線路形式(輸入代碼):	2	半橋式-全波整流/1	半橋式-橋式整流/2
線路形式(輸入代碼):	2	半橋式-全波整流/1	半橋式-橋式整流/2
最大溫升 Δt (°C):	50		
使用Core材	70	3	POT Core(灌狀)/1, 金屬疊片/2, 鐵粉芯/3

環境溫度: **25 °C**

請輸入:	計算結果:					
選材: EI40/27/12	Ap計算值:	6.49386	cm⁴			
Bm: 0.042		PRI	SEC1	SEC2	SEC3	Δt(°C): 55.0
Kj = 590	圈數(T):	6.0	30.5	0.4	0.4	占續率: 37.62 % , 不超過45%.
X = -0.12	線徑(mm):	2.4113	0.943	0.211	0.179	計算得 α: 1.61 %
	線徑修正mm:	1.800	0.900	0.18	0.15	Pcu: 3.214 W
	銅線重量(g):	11.57	14.64	0.01	0.00	Pfe: 0.141 W
	銅阻(Ω):	0.003	0.069	0.020	0.029	
	膚股效應	d <	0.586	mm		
	線徑修正mm:	0.100	0.100	0.36	0.14	
	股數:	324.00	81.00	0.25	1.15	

參考文獻

δ 溫度系數	Weight1	Weight2	Weight3	Weight4	column c1	column c2	column c3	column c4
1.02	0.233271737	0.0583179	0.00233272	0.00162	67.175242	268.70097	6717.5242	9673.2349
Ap	Ac	MLT	Wc	Vol	Wtfe	AS	Ku	Kf
1.6726	1.42	8.22	117.79	9.6276	0.0548	42.03	0.40	4.0

計算步驟:

STEP NO.1: 計算輸出交流電壓

$$E_o = K \cdot V_o + V_d = \begin{matrix} V_{s1} & V_{s2} & V_{s3} \\ 50.6 & 0.6 & 0.6 \\ \hline 51.8 & V & \end{matrix} \quad V$$

STEP NO.2: 計算輸出功率

$$P_{SAC} = E_o \cdot I_o = \begin{matrix} P_{s1} & P_{s2} & P_{s3} \\ 195.973 & 0.116 & 0.084 \\ \hline 196.17 & VA & \\ \hline 250.00 & VA & \end{matrix} \quad VA$$

STEP NO.3: 計算效率

$$\eta = (1 - \alpha) / (1 + \alpha) = 0.945$$

STEP NO.4: 計算總功率(視線路形式而定)

$$P_t \text{ (全波整流)} = P_o \cdot (1/\eta + 2^{0.5}) = 618.01 \quad VA$$

$$P_t \text{ (橋式整流)} = P_o \cdot (1/\eta + 1) = 514.46 \quad VA$$

$$P_t \text{ (無整流)} = P_o \cdot (1/\eta + 1) = 514.46 \quad VA$$

$$P_t(\text{本設計線路}) = 514.456 \text{ VA}$$

STEP NO.6 : 計算鐵芯表面積

$$A_p = [(P_t * 10^4) / (K_f * K_u * K_j * f * B_m)]^{1/(1-X)} = 6.4939 \text{ cm}^4$$

STEP NO.7 : 計算初級圈數

$$N_p = (V_{inmin} * D_{max}) / (2 * B_m * A_c * f) = 6 \text{ T} \quad \text{*** 半橋式工作電壓是輸入電壓的一半}$$

STEP NO.7 : 計算工作週期 D.

$$D_{min} = D_{max} / ((1 - D_{max}) * K + D_{max}) = 0.300 \text{ us}$$

$$D_{max} = K * D_{min} / ((D_{min} * (K - 1) + 1)) = 0.300 \text{ us}$$

STEP NO.8 : 計算初級電流

$$I_p = 2 * (2 * D_{max})^{0.5} * E_o * I_o / V_{inmin} = 25.326 \text{ A}$$

STEP NO.9 : 計算電流密度

$$J = K_j * A_p^X = 554.92 \text{ A/cm}^2$$

STEP NO.10 : 計算初級線徑

$$d_p = 11.287 * (I_p / J)^{1/2} = 2.4113 \text{ mm} \quad \text{輸入修正值: } 1.800 \text{ mm}$$

STEP NO.11 : 計算初級銅阻

$$R_p = MLT * N_p * \text{Column C1} * \delta * 10^{-6} = 0.003 \text{ } \Omega$$

STEP NO.12 : 計算初級銅損

$$P_{cu初} = I_p^2 * R_p = 2.180 \text{ W}$$

STEP NO.13 : 計算次級電流(視電路形式)

	Is1	Is2	Is3	
Is 全波整流 = $(1 + 2D_{max})^{0.5} * I_o =$	3.162	0.158	0.114	A
Is 橋式整流 = $(2 * D_{max})^{0.5} * I_o =$	3.873	0.194	0.139	A
Is 無整流 =	5.000	0.25	0.18	A
Is 本設計線路 =	3.873	0.194	0.139	A

STEP NO.14 : 計算次級圈數

$$N_s = (2 * N_p * E_o * D_{max}) / (V_{inmin} / 2) = \begin{matrix} N_{s1} & N_{s2} & N_{s3} \\ 30.5 & 0.4 & 0.4 \end{matrix} \text{ T}$$

STEP NO.15 : 計算次級線徑

$$d = 11.287 * (I_s / J)^{1/2} = 0.943 \text{ 修正值為 } 0.900 \text{ mm}$$

$$d = 11.287 * (I_s / J)^{1/2} = 0.211 \text{ 修正值為 } 0.180 \text{ mm}$$

$$d = 11.287 * (I_s / J)^{1/2} = 0.179 \text{ 修正值為 } 0.150 \text{ mm}$$

STEP NO. 16 : 銅線占窗面積 :

$$\text{繞線面積 : } N \Phi^2 = N_p^2 * \Phi_1^2 + N_s^2 * \Phi_2^2 = 44.317 \text{ cm}^2$$

$$N \Phi^2(\text{全波整流}) = N_p^2 * \Phi_1^2 + N_s^2 * \Phi_2^2 = 69.15 \text{ cm}^2$$

$$N \Phi^2(\text{橋式整流}) = N_p^2 * \Phi_1^2 + N_s^2 * \Phi_2^2 = 44.32 \text{ cm}^2$$

$$N \Phi^2(\text{無整流}) = N_p^2 * \Phi_1^2 + N_s^2 * \Phi_2^2 = 44.32 \text{ cm}^2$$

$$N \Phi^2 / W_c = 37.62 \%$$

要求: $N \Phi^2 / W_c < 45\%$

STEP NO.17 : 次級銅阻

$$R_s = MLT * N_s * \text{Column C} * \delta * 10^{-6} = \begin{matrix} R_{s1} & R_{s2} & R_{s3} \\ 0.069 & 0.020 & 0.029 \end{matrix} \text{ } \Omega$$

STEP NO.18 : 次級銅損

$$P_{cu次} = I_o^2 * R_s = 1.0335 \text{ W}$$

STEP NO.19 : 總銅損

$$P_{cu} = P_{cu初} + P_{cu次} = 3.2139 \text{ W}$$

STEP NO .20 : 電壓調整率驗算

$$\alpha = P_{cu} / (P_o + P_{cu}) * 100 = 1.61 \%$$

STEP NO.21 : 效率驗算

$$\eta = (1 - \alpha) / (1 + \alpha) = 0.968$$

STEP NO.22 : 允許總損耗

$$P_{\Sigma} = P_o / \eta - P_o = 6.428 \quad \text{W}$$

STEP NO.23 :允許鐵芯損耗

$$P_{fe} = P_{\Sigma} - P_{cu} = 3.2139 \quad \text{W}$$

STEP NO.24 :實際鐵芯損耗

$P_{fe} = 0.165 * 10^{-3} * f^{1.41} * B^{1.77} * W_{tfe} =$	0.1396	W	推挽式
或: $P_{fe} = 0.287 * f^{1.448} * (10 * B)^2 * 10^{-3} * Vol =$	0.1406	W	鐵粉芯 Core
或: $P_{fe} = 0.262 * f^{1.39} * B^{2.19} * 10^{-3} * W_{tfe} =$	0.0471	W	POT Core(灌狀)
或: $P_{fe} = 5.97 * f^{1.26} * B_{ac}^{1.73} * 10^{-3} * W_{tfe} =$	1.1313	W	硅鋼片

本設計線路 $P_{fe} = 0.14061$

STEP NO.25 :實際總損耗

$$P_{\Sigma} = P_{cu} + P_{fe} = 3.355 \quad \text{W}$$

STEP NO.26 :輸出電壓Vo驗算

$V_o = (N_s * V_{inmin}) / (4N_p * D_{max}) - V_d =$	Vs1	Vs2	Vs3	
	50.00	0.00	0.00	V

STEP NO.27.銅線重量

$W_{G1} = MLT * N_p * Weight_1 =$	11.57	g
$W_{G2} = MLT * N_{s1} * Weight_2 =$	14.64	g
$W_{G3} = MLT * N_{s2} * Weight_3 =$	0.01	g
$W_{G4} = MLT * N_{s3} * Weight_4 =$	0.00	g

STEP NO.28.溫升計算.

$$\Delta t = (P_{\Sigma} / (A_s * 0.0005))^{0.79} = 55.01 \quad ^\circ\text{C}$$

STEP NO.29.膚股效應.

$$d < 2 * 65.5 / f^{0.5} = 0.59 \quad \text{mm}$$

STEP NO.30.線圈股數.

PRI : $n = (d / d_{MIN})^2 =$	324.00
SEC1 : $n = (d / d_{MIN})^2 =$	81.00
SEC1 : $n = (d / d_{MIN})^2 =$	0.25
SEC1 : $n = (d / d_{MIN})^2 =$	1.15